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INTERMOUNTAIN POWER SERVICE CORPORATION

April 4, 2001

Richard Sprott, Director
Division of Air Quality
Department of Environmental Quality
P.O. Box 144820
Salt Lake City, UT 84114-4820

Dear Director Sprott,

NOTICE OF INTENT: Modification of Source

Intermountain Power Service Corporation (IPSC) is hereby submitting a Notice of Intent (NOI) to increase generating capacity at the Intermountain Generating Station (IGS) in Delta. The IGS is a coal fired steam-electric plant located in Millard County, a NAAQS Attainment Area. Specifically, IPSC intends to construct modifications to Units One and Two at IGS to enhance performance and reliability and to allow increased capacity by de-bottlenecking certain aspects of our operation. This NOI requests an approval order to construct and a revision to IPSC's Title V permit to incorporate these modifications.

As required by UAC R307-401-2, the following information is provided:

(1) PROCESS DESCRIPTION: IGS is a fossil-fuel fired steam-electric generating station that primarily uses coal as fuel for the production of steam to generate electricity (SIC Code 4911). Both bituminous and subbituminous coals are utilized. Fuel oil and used oil are also combusted for light off and energy recovery.

IGS is a two unit facility operating at a rated capacity of 875 megawatts (MW) per unit (gross). Approximately 5.3 million tons of coal and 600,000 gallons of oil (including used oil) are used each year in the production of electricity. Boiler capacity is rated at 6.2 million pounds per hour of steam flow at 2822 psi.

IGS has in place bulk handling equipment for the unloading, transfer, storage, preparation, and delivery of solid and liquid fuel to the boilers. No changes of this equipment are proposed. No changes in the usage of other raw materials or bulk chemicals are planned.

850 West Brush Wellman Road, Delta, Utah 84624 . Telephone (801) 864-4414 . FAX (801) 864-4970

PROPOSED CHANGES: IPSC is planning to enhance steam flow characteristics through the high pressure (HP) section of each turbine used to generate electricity. This involves the replacement of the HP section with a modified design that improves performance and reliability. This modification in and of itself will not increase plant capacity, but will instead lower emissions due to decreased fuel use from the resulting increased performance.

Combined improvements to other areas of the plant will increase plant generating capacity. These modifications consist of "de-bottlenecking" critical points that presently prevent the full utilization of present equipment. Other changes are needed for reliability, performance and/or routine maintenance purposes. See Item 8 for details.

(2) **EMISSION CHARACTERISTICS:** The composition and physical characteristics of the emissions are expected to change as a result of the proposed modifications as indicated in the attached spreadsheet (Attachment 1), which shows the anticipated changes in emission rates, temperature, air contaminant types, and concentration of air contaminants. The mass flow of chimney effluent may change proportionately with the fuel usage and combustion at a heat input comparable to the current heat input. The existing pollution control devices include low-NOx burners, fabric filters and wet scrubbers.

(3) **POLLUTION CONTROL DEVICE DESCRIPTION:** The existing pollution control device equipment includes dual register low NOx burners, baghouse type fabric filters for particulate removal, and flue gas desulfurization scrubbers. The existing low NOx burners provide a nominal 60% reduction in potential combustion NOx formation, the baghouse filters operate at nominal 99.95% efficiency, and the wet scrubbers operate at nominal 90% efficiency. Control equipment for the handling and transfer of solid material include dust collection filters.

The project includes modifications to the flue gas flow through scrubber modules to enhance SO_2 and acid gas removal rates. Also, the project includes installation of moderately improved NOx controls, such as the replacement of the existing dual register low NOx burners with new technology staged combustion low NOx burners.

(4) **EMISSION POINT**: The present emission point for the IGS boilers is a lined chimney that discharges at 712 feet above ground level (5386 feet above sea level). The chimney location is 39° 39' 39" longitude, 112° 34' 46" latitude (UTM 4374448 meters Northing, 364239 meters Easting.).

(5) **SAMPLING/MONITORING**: Emissions from boiler combustion are continuously sampled and monitored at the chimney for nitrogen oxides, sulfur oxides, carbon dioxide, and volumetric flow. Opacity is measured at the fabric filter outlet. Other parameters recorded include heat input and production level (megawatt load). Monitoring will remain unchanged. Other emissions not directly monitored are calculated using engineering judgement, emission factors, and fuel analyses. The type and location of the monitors will not be changed.

(6) **OPERATING SCHEDULE**: IGS operates 24 hours per day, seven days per week. This will not change as a result of the proposed modifications.

(7) **CONSTRUCTION SCHEDULE**: Construction of the modifications will be performed in a staged manner, generally following the attached schedule. (See Attachment 2.)

(8) **MODIFICATION SPECIFICATIONS**: The changes covered by this NOI include:

- **High Pressure Turbine Retrofit:**
The high pressure turbine on each unit at IGS is scheduled to be replaced with a current technology, high efficiency turbine. This unit will increase high pressure turbine efficiency from approximately 84% to over 92%. Additionally, the turbine will be sized to provide up to 8.6% additional output.

- **Cooling Tower Performance Upgrade:**
The cooling towers on each unit at IGS are scheduled for performance enhancement modifications to increase heat rejection capacity. Also, cooling tower transformers feeding the cooling tower fan motors will be upgraded. A study will be performed to identify and resolve needed redundancy issues for operation at new output levels.

- **Boiler Safety Valve Additions:**
Currently, a review is underway focusing on existing boiler safety valve capacity. Addition of one main steam safety valve on each unit is expected in order to address reliability concerns with the existing valves and to accommodate planned increase in generation capacity.

- **Generator Cooling Enhancement:**
An engineering evaluation is currently underway to identify any enhancements required on the generator in order to accommodate the planned 8.6% increase in generator output. The anticipated result of this evaluation is an upgrade to the current generator and stator cooling systems.

- **Isophase Bus Cooling Enhancement:**
An engineering evaluation is currently underway to identify any enhancements required on the 26kv generator electrical bus feeding the main step-up transformer. The anticipated result of this evaluation is an upgrade to the current isophase bus duct cooling systems.

- **Large Motor Bus Loading Equalization:**
An engineering evaluation is currently underway to equalize the loading between the large and small motor bus. Due to limited tap adjustment capability on the auxiliary transformers feeding these load centers, several motors must be moved from one supply to the other in order to maintain required motor terminal voltages as unit output is increased.

- **Boiler Feed Pump Performance Upgrade:**
The boiler feed pump manufacturer has notified IPSC of several enhancements they now offer that address previous reliability concerns and allow for small increases in output. These include, improved bearing housings, flow path smoothing, and impeller clearance modifications. These modifications provide for increased pump output at acceptable reliability levels.

- **Main Step-up Transformer Cooling:**
The step-up transformer cores currently run close to their nominal temperature ratings when ambient temperatures are high. Proposed modifications are directed at increasing the cooling system capacity for cooling the transformer oil, core, and housing.

- **NOx Reduction Project:**
Some moderate NOx control systems will be added or enhanced. Recent advances in the burner industry have resulted in published operational data with improved NOx removal efficiencies. Within this project, burners in Unit 1 may be replaced with latest technology LNBs. Following successful testing, Unit 2 burner replacements would follow in successive outage upgrades. Alternatively, we may look at other technologies, or a combination of commercially available control systems. The installation of moderate NOx controls is expected to prevent any significant net increases of NOx due to increased capacity.

- **Scrubber Wall Ring:**
Scrubber wall ring technology has been developed and patented in recent years to address inefficient flow patterns that routinely develop within the absorber vessels. This ring would be installed within all twelve (12) scrubber absorber vessels to move flow back to the center of the vessel, providing more efficient SO_2 and acid gas scrubbing of the flue gas.

- **Generator Stator Cooling Water Oxygen Monitoring System:**
Given concerns in recent years regarding the long term integrity of the generator stator bars, an oxygen monitoring system, capable of early identification of stator bar degradation is essential. As load increases, stator bar temperature and cooling flow velocities are also expected to rise. This system will guard against unexpected degradation of the stator.

- **High Pressure Heater Drain Line Modifications:**
An existing resonant vibration occurring in the high pressure heater drain line to the deaerator has become an increasing concern. The vibration appears to increase with load. An increase in unit output would require a modification to eliminate this concern.

- **Boiler Modifications:**

A comprehensive study is currently underway with the manufacturer of the boilers (Babcock & Wilcox). This study has been designed to review all aspects of boiler operation at the new turbine output levels. This study includes evaluation of current technologies and operating practices for minimizing emissions. The study will provide recommendations for modifying the existing boilers for stable and efficient operation at the new higher rating.

- **Circulating Water Makeup Modifications:**

Current circulating water makeup capacity is inadequate for increased unit production. A new design will support increased makeup requirements and return a degree of redundancy to the system, as originally designed.

- **Boiler and turbine control system logic software & controls:**

Upgrade of the existing control system includes complete replacement of the plant information system, control system simulator, coordinated control system, turbine control systems, combustion control systems and the alarm indication system. The new control systems will eliminate parts availability and reliability issues as well as providing the increased control system capacity required for the projects associated with the increased unit output. Boiler and turbine operating parameters are controlled within closer tolerances, resulting in less upsets and better emission control.

The capital expenditures for these changes to both units is expected to be about $35 million. More detailed engineering specifications and project descriptions can be provided as needed.

PRODUCTION SUMMARY: The proposed project will increase generation capacity from 875 to approximately 950 MWhe, with steam flow design increasing from 6.2 to 6.9 million pounds per hour. Design heat input will increase from 8,352 to 9,225 million BTU per hour, requiring an increase from 5.3 to 5.6 million tons of coal each year. See Attachment 1 for details.

- **ADDITIONAL INFORMATION:** IGS operates under a Title V permit (#2700010001). IPSC intends to continue to operate in full compliance with that permit and applicable requirements. No deviations from permit conditions are expected. IPSC requests that this NOI also be considered a request for revision of the Title V permit, and requests that the conditions of the approval order be incorporated into the Title V permit once the approval order is issued.

Operating Flexibility
IPSC reserves the right to cancel any and all planned modifications at any time. IPSC may only install the turbine dense packs, which by themselves would not require review as a major modification. We note that EPA has previously determined that enhancements like the Dense Pack project are not major modifications if there is no significant net increase in emissions. (See letter from Francis X. Lyons, Regional Administrator, EPA Region 5 to Henry Nickel of Hunton & Williams, dated 5/23/00.) If IPSC decides to install only the Dense Pack enhancements and certain upgrades for reliability, IPSC will provide the supporting information to show that there will be no significant net increase in emissions.

Phased Permitting
Due to the length and intermittent nature of the construction schedule for the proposed modifications, IPSC requests that the approval order contain terms that take into account the phases of installation. For example, due to lead times for engineering and budgeting, some portions of the project which affect capacity and/or emissions may be installed prior to upgrades in pollution control equipment. IPSC would be receptive to an approval order that includes interim emission limits for the period prior to project completion and final upgrades to control equipment.

Permit "Off Ramps"
Budgeting for the proposed project will be considered on a fiscal year-by-year basis. Although the current business climate for increased capacity is very favorable for this project, outlooks may change. Accordingly, IPSC proposes that the approval order contain conditions which provide that pollution control upgrades will be required only if those "debottlenecking" projects go forward which, if installed without controls, would increase the potential to emit enough to require major modification review. If IPSC decides not to complete certain portions of this project, the approval order should be structured so that IPSC is not forced to proceed with project completion.

NSPS/PSD Applicability

New Source Performance Standards (NSPS). The proposed modifications do not trigger NSPS applicability under 40 CFR Part 60, Subpart Da. NSPS pollutants for this facility are NOx, SO_2 and PM10. A modification is defined for NSPS purposes to include any change in operation of a source that increases the maximum hourly emissions of a Part 60 regulated pollutant above the maximum achievable rate during the previous five years. See 40 CFR 60.14(h).

Prevention of Significant Deterioration. Planned upgrades to pollution control equipment as part of this proposed modification will result in net emissions decrease for certain criteria pollutants as a result of the project. Other pollutants may have increases below PSD significant levels. Accordingly, this modification will not require a major modification review. IPSC is providing to the DAQ supporting calculations and operating data.

Should you require any additional information, please contact Mr. Dennis Killian, Superintendent of Technical Services, at (435) 864-4414, or dennis-k@ipsc.com.

In as much as this notice of intent also constitutes a request for revision of IPSC's Title V Operating Permit, I hereby certify that, based on information and belief formed after reasonable inquiry, the statements and information in this document and the accompanying attachments are true, accurate, and complete.

Cordially,

S Gale Chapman

S. Gale Chapman
President, Chief Operations Officer, and Title V Responsible Official

Attachments: Excel Spreadsheets (Emissions)
Time Line Project Gantt Chart
IPSC Check, $1,200.00 NOI Fee

cc: Blaine Ipson, IPSC
Jerry Hintze, IPSC
Bruce Moore, LADWP CES
Mike Nosanov, LADWP
Krishna Nand, Parsons Engineering
Reed Searle, IPA
Lynn Banks, IPSC
James Nelson, IPSC
Tim Conkin, LADWP CES
John Schumann, LADWP
James Holtkamp, LLG&M

[redacted]						ATTACHMENT 1: Worksheet A		
NOI / PSD Calculations								
Operating & Production								
Parameter	Average Value	UoM	Post-Change Value					
Rated Output	875	Mwhe	950					
Fuel Use (Coal)	5,264,292	tons/yr	5,578,473					
Plant Operating Time	16,386	Unit hours	16,386					
Heat Value	11,872	BTU/lb	11,872					
Heat Input (Actual)	7,628	MMBtu/hr	8,083					
Heat Input (Design)	8,352	MMBtu/hr	9,225					
Heat Rate	9,564	Btu/KWhr	9,475					
Flow - Stack	125,000,000	scfh	133,000,000					
Emissions					PSD Significance	PSD Major	Difference	PSD
Parameter/Pollutant	2 Yr Average Value	UoM	Post-Change Value	Change+/-	Levels	Trigger Value	(Trigger - Post)	Triggered?
PSD								
SO2	3586.31	Tons	3513.10	-73.21	40	3626.31	-113.21	N
SO2 % Removal	93.62	%	93.88					
NOx	25143.97	Tons	24346.10	-797.87	40	25183.97	-837.87	N
CO	1317.06	Tons	1394.60	77.54	100	1417.06	-22.46	N
PM10	273.77	Tons	283.51	9.75	15	288.77	-5.25	N
Lead	0.087	Tons	0.123	0.036	0.600	0.687	-0.564	N
VOC	12.65	Tons	13.40	0.75	40	52.65	-39.25	N
Beryllium	0.0102	Tons	0.0014	-0.0088	0.0004	0.0106	-0.0092	N
Mercury	0.081	Tons	0.105	0.024	0.100	0.181	-0.076	N
Fluorides (HF)	9.70	Tons	10.16	0.46	3	12.70	-2.54	N
Sulfuric Acid	4.06	Tons	4.05	-0.01	7	11.06	-7.01	N

PSD / NSPS Observations											ATTACHMENT 1: Worksheet B
Plant Emissions [illegible]											
	SO2 (tons)	SO2 % Removal	Nox (tons)	CO (tons)	PM10 (tons)	Lead (lbs)	VOC (lbs)	Beryllium (lbs)	Mercury (lbs)	Fluorides (HF) (lbs)	Sulfuric Acid (lbs)
1996	3759	92.28	19688	1080	83	224		3.57	270	19139	*
1997	5076	92.05	22675	1291	108	263		4.17	323	22905	*
1998	4281	92.67	25708	1321	114	167		2.23	331	23436	8440
1999	3698	93.57	24179	1312	249	156	25394	2.18	123	19167	8234
2000	3474	93.67	26109	1322	299	191	25204	1.89	201	19621	8015
5 Year Avg	4058	92.8	23672	1265	171	200	25299	2.81	250	20854	8230
Last 2 yr Avg	3586	93.6	25144	1317	274	174	25299	2.03	162	19394	8124
TRIGGER: Average + Sig. Incr.	3626		25184	1417	289	1374	105299	2.83	362	25394	22124
Projected Actuals:	3513	93.88	24346	1395	284	245	26809	2.76	211	20313	8108

Plant Operations [illegible]	Coal Usage (tons)	Plant Operating Hours	Btu/lb Coal HV	MBTU/hr Avg Heat Input	LB/MMBtu NOx Emission rate	lbs/hr NOx Emission Rate	LB/MMBtu SO2 Emission Rate	lbs/hr SO2 Emission Rate		Maximum NOx Emission Rate (Last 5 years)	Maximum SO2 Emission Rate (Last 5 years)
1996	4310562	15359	11860	6657	0.39	2564	0.07	489		6045	1150
1997	5158867	16564	11789	7343	0.37	2738	0.08	613		4875	1333
1998	5278344	16683	11823	7481	0.41	3082	0.07	513		5331	1279
1999	5244793	16462	11858	7556	0.39	2938	0.06	449		5007	1456
2000	5283790	16309	11885	7701	0.42	3202	0.06	426		5441	1379
5 Year Avg	5055271	16275	11843	7348	0.39	2905	0.07	498	**Max.-Prev. 5 yrs.**	6045	1456
Last 2 Year Avg	5264292	16386	11872	7628	0.40	3070	0.06	438	**Proposed Average:**	2972	429
Projected Actuals:	5578473	16386	11843	8064	0.37	2972	0.05	429	**Proposed Max:**	4613	1384

OPERATING CHANGES	Actual Max Heat Input	Design Max Heat Input (MMBtu/hr)	Fuel Use (coal, tons)	Heat Rate	Mlbs/hr Steam	Mwhe	Stack Flow (scfh)
Present Operation	7628	8352	5264291.5	9564	6.1	875	125,000,000
Proposed Operation	8083	9225	5,578,473	9475	6.9	950	133,000,000

ASSUMPTIONS:

All increases / decreases based on coal use only. Fuel oil & other bulk chemical chemical use not expected to change.
Estimated 15% nominal reduction with new NOx controls over old.
Estimated 4% nominal removal eflciciency improvement in scrubber efficiency.
HAPs PSD triggers calculated per UDAQ Dispersion Modeling Guidelines at R307-410-4.
VOC's calculated from HAPs list.
Projected nominal efficiency improvement: 8.0%
Projected nominal capacity improvement: 8.6%
Projected heat input / coal usage increase: 5.9%
Projected uncontrolled NOx increase: 11.2%

HAPs / Other Projection Data

POLLUTANT	Concentration (ppm)	Pollutant Emission Factor (lbs/10^12 Btu)	Control Device Efficiency (CE) (% emission of fuel conc.)	Table or Method Used*	Actual Emission Factor (EF)	Calculation
[illegible]						
Antimony	3.1	0.92*(C/A*PM)^0.63		AP-42 1.1-15	0.300	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Arsenic	12	3.1*(C/A*PM)^0.85		AP-42 1.1-15	2.157	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Barium	113	(C/A*PM)		Eng. Calc.(1)	6.147	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Beryllium	0.38	1.2*(C/A*PM)^1.1		AP-42 1.1-15	0.017	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Cadmium	0.66	3.3*(C/A*PM)^0.5		AP-42 1.1-15	0.625	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Chromium	24	3.7*(C/A*PM)^0.58		AP-42 1.1-15	4.319	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Cobalt	2.9	1.7*(C/A*PM)^0.69		AP-42 1.1-15	0.475	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Copper	7.8	(C/A*PM)		Eng. Calc.(1)	0.424	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Lead	7.1	3.4*(C/A*PM)^0.80		AP-42 1.1-15	1.588	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Manganese	9.9	3.8*(C/A*PM)^0.60		AP-42 1.1-15	2.621	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Mercury	0.061		31%	Eng. Calc.(2)		E=ConcHg(ppm)*Thruput(Mtons)*Control Efficency(CE)*2000lbs/ton
Nickel	4.7	4.4*(C/A*PM)^0.48		AP-42 1.1-15	2.286	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Selenium	2.4		12%	Eng. Calc.(3)		E=ConcHg(ppm)*Thruput(Mtons)*Control Efficiency(CE)*2000lbs/ton
Vanadium	5.6	(C/A*PM)		Eng. Calc.(1)	0.305	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Zinc	7.4	(C/A*PM)		Eng. Calc.(1)	0.403	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
[illegible]						
Acenaphthene		0.00000051 (lbs/ton)		AP-42 1.1-12	5.10E-07	E=EF(lbs/ton)*Thruput(tons)
Acenaphthylene		2.5E-07 (lbs/ton)		AP-42 1.1-12	2.50E-07	E=EF(lbs/ton)*Thruput(tons)
Acetaldehyde@		0.00057 (lbs/ton)		AP-42 1.1-13	5.70E-04	E=EF(lbs/ton)*Thruput(tons)
Acetophenone@		0.000015 (lbs/ton)		AP-42 1.1-13	1.50E-05	E=EF(lbs/ton)*Thruput(tons)
Acrolein@		0.00029 (lbs/ton)		AP-42 1.1-13	2.90E-04	E=EF(lbs/ton)*Thruput(tons)
Anthracene		0.00000021 (lbs/ton)		AP-42 1.1-12	2.10E-07	E=EF(lbs/ton)*Thruput(tons)
Benzene@		3.8 (lbs/10^12 BTU)		Eng. Calc.(3)	3.80E+00	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Benzo(a)anthracene		8.0E-08 (lbs/ton)		AP-42 1.1-12	8.00E-08	E=EF(lbs/ton)*Thruput(tons)
Benzo(a)pyrene		0.0018 (lbs/10^12 BTU)		Eng. Calc.(3)	1.80E-03	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Benzo(b,j,k)Fluoranthene		1.1E-07 (lbs/ton)		AP-42 1.1-12	1.10E-07	E=EF(lbs/ton)*Thruput(tons)
Benzo(g,h,i)perylene		2.7E-08 (lbs/ton)		AP-42 1.1-12	2.70E-08	E=EF(lbs/ton)*Thruput(tons)
Benzyl chloride@		0.0007 (lbs/ton)		AP-42 1.1-13	7.00E-04	E=EF(lbs/ton)*Thruput(tons)
Biphenyl@		0.0000017 (lbs/ton)		AP-42 1.1-12	1.70E-06	E=EF(lbs/ton)*Thruput(tons)
Bis(2-ethylhexyl)phthalate (DEHP)@		0.000073 (lbs/ton)		AP-42 1.1-13	7.30E-05	E=EF(lbs/ton)*Thruput(tons)
Bromoform@		0.000039 (lbs/ton)		AP-42 1.1-13	3.90E-05	E=EF(lbs/ton)*Thruput(tons)
Carbon disulfide@		0.00013 (lbs/ton)		AP-42 1.1-13	1.30E-04	E=EF(lbs/ton)*Thruput(tons)
2-Chloroacetophenone@		0.000007 (lbs/ton)		AP-42 1.1-13	7.00E-06	E=EF(lbs/ton)*Thruput(tons)
Chlorobenzene@		0.000022 (lbs/ton)		AP-42 1.1-13	2.20E-05	E=EF(lbs/ton)*Thruput(tons)
Chloroform@		0.000059 (lbs/ton)		AP-42 1.1-13	5.90E-05	E=EF(lbs/ton)*Thruput(tons)
Chrysene		0.0000001 (lbs/ton)		AP-42 1.1-12	1.00E-07	E=EF(lbs/ton)*Thruput(tons)
Cumene@		0.0000053 (lbs/ton)		AP-42 1.1-13	5.30E-06	E=EF(lbs/ton)*Thruput(tons)
Cyanide		0.0025 (lbs/ton)		AP-42 1.1-13	2.50E-03	E=EF(lbs/ton)*Thruput(tons)
2,4-Dinitrotoluene@		0.00000028 (lbs/ton)		AP-42 1.1-13	2.80E-07	E=EF(lbs/ton)*Thruput(tons)
Dimethyl sulfate@		0.000048 (lbs/ton)		AP-42 1.1-13	4.80E-05	E=EF(lbs/ton)*Thruput(tons)
Ethyl benzene@		0.000094 (lbs/ton)		AP-42 1.1-13	9.40E-05	E=EF(lbs/ton)*Thruput(tons)
Ethyl chloride@		0.000042 (lbs/ton)		AP-42 1.1-13	4.20E-05	E=EF(lbs/ton)*Thruput(tons)
Ethylene dichloride@		0.00004 (lbs/ton)		AP-42 1.1-13	4.00E-05	E=EF(lbs/ton)*Thruput(tons)
Ethylene dibromide@		0.0000012 (lbs/ton)		AP-42 1.1-13	1.20E-06	E=EF(lbs/ton)*Thruput(tons)
Fluoranthene		0.00000071 (lbs/ton)		AP-42 1.1-12	7.10E-07	E=EF(lbs/ton)*Thruput(tons)
Fluorene		9.1E-07 (lbs/ton)		AP-42 1.1-12	9.10E-07	E=EF(lbs/ton)*Thruput(tons)
Formaldehyde@		3.0 (lbs/10^12 BTU)		Eng. Calc.(3)	3.00E+00	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Hexane@		0.000067 (lbs/ton)		AP-42 1.1-13	6.70E-05	E=EF(lbs/ton)*Thruput(tons)
Indeno(1,2,3-cd)pyrene		6.1E-08 (lbs/ton)		AP-42 1.1-12	6.10E-08	E=EF(lbs/ton)*Thruput(tons)
Isophorone@		0.00058 (lbs/ton)		AP-42 1.1-13	5.80E-04	E=EF(lbs/ton)*Thruput(tons)
Methyl bromide@		0.00016 (lbs/ton)		AP-42 1.1-13	1.60E-04	E=EF(lbs/ton)*Thruput(tons)
Methyl chloride@		0.00053 (lbs/ton)		AP-42 1.1-13	5.30E-04	E=EF(lbs/ton)*Thruput(tons)
5-Methyl chrysene		2.2E-08 (lbs/ton)		AP-42 1.1-12	2.20E-08	E=EF(lbs/ton)*Thruput(tons)
Methyl ethyl ketone@		0.00039 (lbs/ton)		AP-42 1.1-13	3.90E-04	E=EF(lbs/ton)*Thruput(tons)
Methyl hydrazine@		0.00017 (lbs/ton)		AP-42 1.1-13	1.70E-04	E=EF(lbs/ton)*Thruput(tons)
Methyl methacrylate@		0.00002 (lbs/ton)		AP-42 1.1-13	2.00E-05	E=EF(lbs/ton)*Thruput(tons)
Methyl tert butyl ether@		0.000035 (lbs/ton)		AP-42 1.1-13	3.50E-05	E=EF(lbs/ton)*Thruput(tons)
Methylene chloride		0.00029 (lbs/ton)		AP-42 1.1-13	2.90E-04	E=EF(lbs/ton)*Thruput(tons)
Naphthalene@		0.000013 (lbs/ton)		AP-42 1.1-12	1.30E-05	E=EF(lbs/ton)*Thruput(tons)
Phenanthrene		0.0000027 (lbs/ton)		AP-42 1.1-12	2.70E-06	E=EF(lbs/ton)*Thruput(tons)
Phenol@		0.000016 (lbs/ton)		AP-42 1.1-13	1.60E-05	E=EF(lbs/ton)*Thruput(tons)
Propionaldehyde@		0.00038 (lbs/ton)		AP-42 1.1-13	3.80E-04	E=EF(lbs/ton)*Thruput(tons)
Pyrene		0.00000033 (lbs/ton)		AP-42 1.1-12	3.30E-07	E=EF(lbs/ton)*Thruput(tons)
Tetrachloroethylene		0.000043 (lbs/ton)		AP-42 1.1-13	4.30E-05	E=EF(lbs/ton)*Thruput(tons)
Toluene@		1.4 (lbs/10^12 BTU)		Eng. Calc.(3)	1.40E+00	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
1,1,1-Trichloroethane		0.00002 (lbs/ton)		AP-42 1.1-13	2.00E-05	E=EF(lbs/ton)*Thruput(tons)
Styrene@		0.000025 (lbs/ton)		AP-42 1.1-13	2.50E-05	E=EF(lbs/ton)*Thruput(tons)
Xylenes@		0.000037 (lbs/ton)		AP-42 1.1-13	3.70E-05	E=EF(lbs/ton)*Thruput(tons)
Vinyl acetate@		0.0000076 (lbs/ton)		AP-42 1.1-13	7.60E-06	E=EF(lbs/ton)*Thruput(tons)
[illegible]						
Total PCDD/PCDF		0.000002 (lbs/10^12 BTU)		Eng. Calc.(3)	2.00E-06	E=[EF(lbs/10^12 Btu)*Thruput(tons)*2000lbs/ton*HV(Btu/lb)]/10^12
Acid Gases						
Hydrogen Chloride	299		3%	Eng. Calc.(3)		E=Conc(ppm)*Thruput(Mtons)*Control Efficiency(CE)*2000lbs/ton
Hydrogen Fluoride	63		3%	Eng. Calc.(3)		E=Conc(ppm)*Thruput(Mtons)*Control Efficiency(CE)*2000lbs/ton
Sulfuric Acid	0.50%	0.0646 (lbs/ton)	4.50%	Eng. Calc.(4)	0.0645986	E=EF(lbs/ton)*Thruput(tons)*Conc(%)*100*Control Efficiency(CE)

POLLUTANT	Projected Emissions (lbs/yr)	MW	ACGIH Class	z	Previous Actuals 1999	2000	Average	Change +/-	Release Rate	ACGIH TLV	Units	ETF	ETV	TSL	Difference	Modeling Review?
Antimony	39.70		Chronic	30	35.249686	35.22769636	35.23869118	4.47	0.0002725	0.5	mg/m3	0.368	0.184	0.016666667	-0.1837275	
Arsenic	285.75		A1	90	271.4042005	259.7689862	265.5865933	20.16	0.001230335	0.01	mg/m3	0.123	0.00123	0.000111111	3.34976E-07	Y
Barium	814.20				686.1213449	611.2064079	648.6638764	165.54	0.010102368							
Beryllium	2.23		A1	90	1.878347314	2.179624581	2.028985948	0.20	1.22205E-05	0.002	mg/m3	0.123	0.000246	2.22222E-05	-0.00023378	
Cadmium	82.82		A2	90	74.3726225	62.1744665	68.2735445	14.55	0.000887876	0.01	mg/m3	0.123	0.00123	0.000111111	-0.000342124	
Chromium	572.05		A1	90	534.0143915	524.299845	529.1571183	42.89	0.002617514	0.05	mg/m3	0.123	0.00615	0.000555556	-0.003532486	
Cobalt	62.97		Chronic	30	55.73090035	53.55300623	54.64195329	8.33	0.000508172	0.02	mg/m3	0.368	0.00736	0.000666667	-0.006851828	
Copper	56.20				52.4658637	33.13198938	42.79892654	13.40	0.000817929							
Lead	210.39		Chronic	30	190.6875338	156.0387354	173.3631346	37.03	0.002259576	0.05	mg/m3	0.368	0.0184	0.001666667	-0.016140424	
Manganese	347.20		Chronic	30	334.4265091	251.099068	292.7627885	54.44	0.003322407	0.1	mg/m3	0.368	0.0368	0.003333333	-0.033477593	
Mercury	210.98		Chronic	30	201.0140415	123.4200948	162.2170682	48.76	0.002975759	0.025	mg/m3	0.368	0.0092	0.000833333	-0.008224241	
Nickel	302.84		Chronic	30	322.8089641	270.9079077	296.8584359	5.98	0.000364871	0.1	mg/m3	0.368	0.0368	0.003333333	-0.036435129	
Selenium	3213.20		Chronic	30	3035.360736	3393.982104	3214.67142	-1.47	-8.977E-05	0.2	mg/m3	0.368	0.0736	0.006666667	-0.07368977	
Vanadium	40.35				771.6565463		771.6565463	-731.31	-0.044629974							
Zinc	53.32				50.13591069	44.30573506	47.22082287	6.10	0.000372181							
Acenaphthene	2.85				2.6947329	2.67484443	2.684788665	0.16	9.77863E-06							
Acenaphthylene	1.395				1.3209475	1.31119825	1.316072875	0.08	4.79344E-06							
Acetaldehyde@	3,179.73	44.05	Acute	10	3011.7603	2989.53201	3000.646155	179.08	0.010929053	25	ppm C	0.31	13.96267894	4.50408998	-13.95174988	
Acetophenone@	83.88	120.15	Chronic	30	79.25685	78.671895	78.9643725	4.71	0.000287607	10	ppm	0.368	18.08392638	1.63803681	-18.08363877	
Acrolein@	1,617.76	56.06	Acute	10	1532.2991	1520.98997	1526.644535	91.11	0.005560395	0.1	ppm C	0.31	0.071078119	0.022928425	-0.065517723	
Anthracene	1.171				1.1095959	1.10140653	1.105501215	0.07	4.02649E-06							
Benzene@	503.33	78.11	Chronic	30	477.5258698	472.828236	475.1770529	28.15	0.00171811	0.5	ppm	0.368	0.587821677	0.053244717	-0.586103567	
Benzo(a)anthracene	0.446				0.4227032	0.41958344	0.42114332	0.03	1.5339E-06							
Benzo(a)pyrene	0.238				0.226196465	0.22397127	0.225083867	0.01	8.13841E-07							
Benzo(b,j,k)Fluoranthene	0.614				0.5812169	0.57692723	0.579072065	0.03	2.10912E-06							
Benzo(g,h,i)perylene	0.151				0.14266233	0.141609411	0.142135871	0.01	5.17692E-07							
Benzyl chloride@	3,904.93	126.58	Chronic	30	3698.653	3671.3551	3685.00405	219.93	0.013421643	1	ppm	0.368	1.90517137	0.17256987	-1.891749727	
Biphenyl@	9.48	154.2	Chronic	30	8.982443	8.9161481	8.94929555	0.53	3.25954E-05	0.2	ppm	0.368	0.464176687	0.04204499	-0.464144092	
Bis(2-ethylhexyl)phthalate (DEHP)@	407.23				385.71667	382.869889	384.2932795	22.94	0.001399686							
Bromoform@	217.56	252.8	Chronic	30	206.06781	204.546927	205.3073685	12.25	0.000747777	0.5	ppm	0.368	1.902462168	0.172324472	-1.90171439	
Carbon disulfide@	725.20	76.14	Chronic	30	686.8927	681.82309	684.357895	40.84	0.002492591	10	ppm	0.368	11.45992638	1.03803681	-11.45743379	
2-Chloroacetophenone@	39.05	154.59	Chronic	30	36.98653	36.713551	36.8500405	2.20	0.000134216	0.05	ppm	0.368	0.116337669	0.010537832	-0.116203452	
Chlorobenzene@	122.73	112.56	Chronic	30	116.24338	115.385446	115.814413	6.91	0.000421823	10	ppm	0.368	16.94154601	1.534560327	-16.94112419	
Chloroform@	329.13	119.38	Chronic	30	311.74361	309.442787	310.5931985	18.54	0.001131253	10	ppm	0.368	17.96803272	1.627539196	-17.96690147	
Chrysene	0.558	228.3	Chronic	30	0.528379	0.5244793	0.52642915	0.03	1.91738E-06	L	ppm	0.368	#VALUE!	#VALUE!	#VALUE!	
Cumene@	29.57	120.19	Chronic	30	28.004087	27.7974029	27.90074495	1.67	0.000101621	50	ppm	0.368	90.44973415	8.192910702	-90.44963253	
Cyanide	13,946.18				13209.475	13111.9825	13160.72875	795.45	0.047934441							
2,4-Dinitrotoluene@	1.562				1.4794612	1.46854204	1.47400162	0.09	5.36866E-06							
Dimethyl sulfate@	267.77	126.1	Chronic	30	253.62192	251.750064	252.685992	15.08	0.000920341	0.1	ppm	0.368	0.189794683	0.017191547	-0.188874342	
Ethyl benzene@	524.38	106.16	Chronic	30	496.67626	493.010542	494.843401	29.53	0.001802335	100	ppm	0.368	159.7827403	14.4730743	-159.780938	
Ethyl chloride@	234.30	64.52	Chronic	30	221.91918	220.281306	221.100243	13.20	0.000805299	100	ppm	0.368	97.10985685	8.796182686	-97.10905155	
Ethylene dichloride@	223.14	98.96	Chronic	30	211.3516	209.79172	210.57166	12.57	0.000766951	10	ppm	0.368	14.89459305	1.349147921	-14.8938261	
Ethylene dibromide@	6.69	187.88	Chronic	30	6.340548	6.2937516	6.3171498	0.38	2.30085E-05	L	ppm	0.368	#VALUE!			
Fluoranthene	3.96				3.7514909	3.72380303	3.737646965	0.22	1.36134E-05							
Fluorene	5.08				4.8082489	4.77276163	4.790505265	0.29	1.74481E-05							
Formaldehyde@	397.37	30.03	Acute / A2	90	376.9941077	373.2854495	375.1397786	22.23	0.001356402	0.3	ppm	0.123	0.04532135	0.00409407	-0.043964947	
Hexane@	373.76	86.18	Chronic	30	354.01393	351.401131	352.7075305	21.05	0.001284643	500	ppm	0.368	648.5529652	58.7457396	-648.5516806	
Indeno(1,2,3-cd)pyrene	0.340				0.32231119	0.319932373	0.321121782	0.02	1.1696E-06							
Isophorone@	3,235.51	138.21	Acute	10	3064.5982	3041.97994	3053.28907	182.23	0.01112079	5	ppm	0.31	8.761779141	2.826380368	-8.750658351	
Methyl bromide@	892.56	94.95	Chronic	30	845.4064	839.16688	842.28664	50.27	0.003067804	1	ppm	0.368	1.429104294	0.129447853	-1.42603649	
Methyl chloride@	2,956.59	50.49	Chronic	30	2800.4087	2779.74029	2790.074495	156.52	0.010162101	50	ppm	0.368	37.99656442	3.441717791	-37.98640232	
5-Methyl chrysene	0.123				0.11624338	0.115385446	0.115814413	0.01	4.21823E-07							
Methyl ethyl ketone@	2,175.60	72.1	Chronic	30	2060.6781	2045.46927	2053.073685	122.53	0.007477773	200	ppm	0.368	217.0372188	19.65916837	-217.029741	
Methyl hydrazine@	948.34	46.07	Chronic	30	898.2443	891.61481	894.929555	53.41	0.003259542	0.01	ppm	0.368	0.006934053	0.000628085	-0.003674511	
Methyl methacrylate@	111.57	100.13	Chronic	30	105.6758	104.89586	105.28583	6.28	0.000383476	50	ppm	0.368	75.35345603	6.825494206	-75.35307258	
Methyl tert butyl ether@	195.25	88.17	Chronic	30	184.93265	183.567755	184.2502025	11.00	0.000671082	40	ppm	0.368	53.08230675	4.808179959	-53.08163567	
Methylene chloride	1,617.76	84.93	Chronic	30	1532.2991	1520.98997	1526.644535	91.11	0.005560395	50	ppm	0.368	63.91460123	5.789366053	-63.90904083	
Naphthalene@	72.52	128.19	Chronic	30	68.68927	68.182309	68.4357895	4.08	0.000249259	10	ppm	0.368	19.29403681	1.747648262	-19.29378755	
Phenanthrene	15.06				14.266233	14.1609411	14.21358705	0.85	5.17692E-05							
Phenol@	89.26	94.11	Chronic	30	84.54064	83.916688	84.228664	5.03	0.00030678	5	ppm	0.368	7.082306748	0.641513292	-7.081999968	
Propionaldehyde@	2,119.82				2007.8402	1993.02134	2000.43077	119.39	0.007286035							
Pyrene	1.841				1.7436507	1.73078169	1.737216195	0.10	6.32735E-06							
Tetrachloroethylene	239.87	165.8	Chronic	30	227.20297	225.526099	226.3645345	13.51	0.000824472	25	ppm	0.368	62.38691207	5.650988412	-62.38608759	
Toluene@	185.44	92.13	Chronic	30	175.9305836	174.1998764	175.06523	10.37	0.000632988	50	ppm	0.368	69.33300613	6.280163599	-69.33237315	
1,1,1-Trichloroethane	111.57	133.42	Chronic	30	105.6758	104.89586	105.28583	6.28	0.000383476	350	ppm	0.368	702.8423722	63.66325835	-702.8419887	
Styrene@	139.46	104.16	Chronic	30	132.09475	131.119825	131.6072875	7.85	0.000479344	20	ppm	0.368	31.35450307	2.8400818	-31.35402372	
Xylenes@	206.40	106.16	Chronic	30	195.50023	194.057341	194.7787855	11.62	0.00070943	100	ppm	0.368	159.7827403	14.4730743	-159.7820309	
Vinyl acetate@	42.40	86.09	Chronic	30	40.156804	39.8604268	40.0086154	2.39	0.000145721	10	ppm	0.368	12.95751329	1.173687798	-12.95736757	
[illegible]	26569.0441				25167.22598	24978.94757	25073.08678									
Total PCDD/PCDF	264.9E-6				0.000251329	0.000248857	0.000250093	0.00	9.04268E-10							
Hydrogen Chloride	96,408.29				96912.55014	95576.89842	96244.72428	163.56	0.009981802							
Hydrogen Fluoride	20,313.45				19621.02804	19166.91888	19393.97346	919.48	0.056113641							
Sulfuric Acid	8,108.13				7994.561802	8215.776742	8105.169272	2.97	0.000180978							

Notes
(1) By ash fraction derivative
(2) By stack test
(3) By EPRI's Trace Report
(4) By SoCo's Paper
Realized HAP emission increases calculated per Utah R307-410-4.
To convert ppm to mg/m3: TLV(ppm) X MW / 24.45
z = impact (acute/chronic/carcinogenic)
ETF = Emission Threshold Factor (Table IV-2, R307-410-4, Boundaries >100m)
TLV = Threshold Limit Values (ACGIH 2001 version)
ETV = Emission Threshold Value ([lb/hr] = [TLV] X [ETF])
TSL = Toxic Screening Level (TLV/z)
MW = Atomic molecular weight of compound
@ = VOC

Coal Throughput = 5,578,473 tons
Heating Value = 11,872 Btu/lb
Ash = 8.64%
Plant operating hours = 16,386
Fabric Filter Efficiency = 0.0047 lbs/MMBtu

	HP TURBINE DENSE PACK SO2 PROJECTIONS				**ATTACHMENT 1**: Worksheet D			
	99-00 Average lbs/mmbtu							
	inlet	stack	% reduction					
	0.7744	**0.0494**	**93.6209**		U1/U2 '99-00 average			
	0.7744	**0.0474**	93.8760		4% reduction stack lbs/mmbtu			
	0.7744	0.0204	97.3657		97.3657% reduction (4% increase in scrubber efficiency)			
	1999							
	Unit One				Unit Two			
	Coal Burned (tons)	2,472,213			Coal Burned (tons)	2,772,580		
	Heating Value btu/lb	11,858			Heating Value btu/lb	11,858		
	Inlet SO2 lbs/mmbtu	0.7963			Inlet SO2 lbs/mmbtu	0.7867		
	Stack SO2 lbs/mmbtu	0.0479			Stack SO2 lbs/mmbtu	0.0538		
	Inlet Tons SO2	23,343.93			Inlet Tons SO2	25,864.54		
	Stack Tons SO2	1,404.21	1,566.40	(EDR)	Stack Tons SO2	1,768.80	[illegible]	(EDR)
	% Removal (lbs/mmbtu)	93.9847			% Removal (lbs/mmbtu)	93.1613		
	% Removal (tons)	93.9847			% Removal (tons)	93.1613		
	% Removal (EDR tons)	93.2899	0.69		% Removal (EDR tons)	91.7578	1.40	
	2000							
	Unit One				Unit Two			
	Coal Burned (tons)	2,799,081			Coal Burned (tons)	2,484,709		
	Heating Value btu/lb	11,885			Heating Value btu/lb	11,885		
	Inlet SO2 lbs/mmbtu	0.7712			Inlet SO2 lbs/mmbtu	0.7432		
	Stack SO2 lbs/mmbtu	0.0482			Stack SO2 lbs/mmbtu	0.0477		
	Inlet Tons SO2	25,655.57			Inlet Tons SO2	21,947.27		
	Stack Tons SO2	1,603.47	1,855.40	(EDR)	Stack Tons SO2	1,408.62	[illegible]	(EDR)
	% Removal (lbs/mmbtu)	93.7500			% Removal (lbs/mmbtu)	93.5818		
	% Removal (tons)	93.7500			% Removal (tons)	93.5818		
	% Removal (EDR tons)	92.7692	0.98		% Removal (EDR tons)	92.6223	0.96	
	1999-2000 Average Intermountain Generating Station							
	% Removal (lbs/mmbtu)	93.6194			Inlet lbs/mmbtu	**0.7744**		
	% Removal (tons)	93.6194			Stack lbs/mmbtu	**0.0494**		
	% Removal (EDR tons)	92.6098	1.01					
	Dense Pack - Intermountain Generating Station							
	PREMODIFICATION	1999 - 2000 Average (calculated)			POST MODIFICATION (W/O Scrubber Modification)			
	Coal Burned (tons)	5,268,249			Coal Burned (tons)	5,578,473		
	Heating Value btu/lb	11,871			Heating Value btu/lb	11,871		
	Inlet SO2 lbs/mmbtu	**0.7744**			Inlet SO2 lbs/mmbtu	**0.7744**		
	Stack SO2 lbs/mmbtu	**0.0494**			Stack SO2 lbs/mmbtu	**0.0494**		
	Inlet Tons SO2	48,430.50	54,170.45	Actual	Inlet Tons SO2	51,282.36	57403.69	Actual Projected
	Stack Tons SO2	3,089.45	3586.25	(EDR)	Stack Tons SO2	3,271.37	3797.87	(EDR Projected)
	% Removal (lbs/mmbtu)	93.6209	93.38		% Removal (lbs/mmbtu)	93.6209	93.68	
					POST MODIFICATION (W/Scrubber Modification)			
		Tons of SO2 Reduction			4% reduction stack lbs/mmbtu			
		130.85			Coal Burned (tons)	5,578,473		
		273.15	(EDR Projected)		Heating Value btu/lb	11,871		
					Inlet SO2 lbs/mmbtu	**0.7744**		
					Stack SO2 lbs/mmbtu	**0.047424**		
					Inlet Tons SO2	51,282.36	57403.69	Actual Projected
					Stack Tons SO2	3,140.51	3,513.10	(EDR Projected)
					% Removal (lbs/mmbtu)	93.8760	93.88	
					POST MODIFICATION (W/Scrubber Modification)			
		Tons of SO2 Reduction			97.3657% reduction (4% increase in scrubber efficiency)			
		1,920.44			Coal Burned (tons)	5,578,473		
		2074.06	(EDR Projected)		Heating Value btu/lb	11,871		
					Inlet SO2 lbs/mmbtu	**0.7744**		
					Stack SO2 lbs/mmbtu	0.0204		
					Inlet Tons SO2	51,282.36	57403.69	Actual Projected
					Stack Tons SO2	1,350.93	1,512.19	(EDR Projected)
					% Removal (lbs/mmbtu)	97.3657		
NOTES:								
1	Stack SO2 tons calculated from lbs/mmbtu are less than SO2 tons calculated for EDR from CEM SO2 ppm and Stack flow.							
2	Dense Pack SO2 tons are calculated from lbs/mmbtu. (yellow boxes)							

ATTACHMENT 1: Worksheet E

CO Calculations

Dense Pack - Intermountain Generating Station			
PREMODIFICATION	1999 - 2000 Average	POST MODIFICATION	
Coal Burned (tons)	5,268,249	Coal Burned (tons)	5,578,473
CO E.F. (lb/ton)	0.50	CO E.F. (lb/ton)	0.50
CO Emissons (tons)	1317.06	CO Emissons (tons)	1394.62

Tons of CO increase
77.56

AP-42 Table 1.1-3

DENSE PACK PM10
COAL USAGE CALCULATION SUMMARY

ATTACHMENT 1: Worksheet F

YEARLY INVENTORY

5,578,473	Tons coal received Railcar Unloading
5,578,473	Tons of coal fed to both Units
2,789,237	Tons of coal fed to Unit 1
2,789,237	Tons of coal fed to Unit 2
11,800	Coal heating value (Btu/lb)
25.1	Coal pile (acres)
0.0056	Unit 1 Particulate lbs/mmbtu (tsp)
0.0036	Unit 2 Particulate lbs/mmbtu (tsp)

UNIT 1 FABRIC FILTER PARTICULATE EMISSION (online)
169.5677 TPY Particulate PM10 — AP 42 Table 1.1-6

UNIT 2 FABRIC FILTER PARTICULATE EMISSION (online)
109.0078 TPY Particulate PM10 — AP 42 Table 1.1-6

COAL TRAIN UNLOADING DUST COLLECTORS A,B,C,D
0.0625 TPY Particulate PM10

COAL TRUCK UNLOADING DUST COLLECTOR
0.0000 TPY Particulate PM10 — Included in train unloading

COAL RESERVE RECLAIM DUST COLLECTOR
0.0020 TPY Particulate PM10 — 10% of Coal Crusher Emissions

COAL SAMPLE PREPARATION DUST COLLECTOR
0.0000 TPY Particulate PM10

COAL TRANSFER BUILDING #1 DUST COLLECTOR
0.0156 TPY Particulate PM10

COAL TRANSFER BUILDING #2 DUST COLLECTOR
0.0312 TPY Particulate PM10

COAL TRANSFER BUILDING #4 DUST COLLECTOR
0.0195 TPY Particulate PM10

COAL CRUSHER BUILDING DUST COLLECTOR
0.0195 TPY Particulate PM10

ACTIVE COAL STACKOUT (fugitive)
3.9049 TPY Particulate PM10

DUST COLLECTOR 13A & 13B
0.0312 TPY Particulate PM10

DUST COLLECTOR 14A & 14B
0.0156 TPY Particulate PM10

COAL PILE FUGITIVE EMISSIONS
0.8368 TPY Particulate PM10

283.5145 TPY PM10 (COAL ONLY)

COMMENTS
EF found in AP-42 Table 11.19.2-1 site dust collectors for coal, limestone, lime vacuum sys. and soda ash PM10 and PM2.5.
Using same ratio of PM10 to PM2.5 found with emissions at stack.
Use cumulative Mass % <= Stated Size in AP-42 Table 1.1-5 for percentages of PM10 and PM2.5 as a ratio of TSP.
PM10 = 92% of TSP
PM2.5 = 53% of TSP

ATTACHMENT 2

IGS Uprate Project Coordination

Task Name	Start	Finish
Unit 2 Projects	1/2/2001	4/1/2004
HP Turbine Retrofit	1/15/2001	4/1/2002
Cooling Tower Performance Upgrade	2/1/2001	4/1/2004
Boiler Safety Valve Addition	4/2/2001	4/1/2002
Generator Cooling Enhancements	4/2/2001	4/1/2002
Isophase Cooling Enhancements	4/2/2001	4/1/2002
Large Motor Bus Loading Equalization	4/2/2001	4/1/2002
Boiler Feed Pump Performance Upgrade	1/2/2001	4/1/2003
Main Step-up Transformer Cooling	3/1/2001	4/1/2002
NOx Reduction Project	4/2/2001	4/1/2004
Scrubber Wall Ring	5/2/2001	4/2/2003
Generator SCW O2 Monitoring	4/2/2001	4/1/2002
HP Heater Drain Line Mods	4/2/2001	4/1/2002
Boiler Modifications	4/2/2001	4/1/2004
Cooling Tower Makeup Modifications	1/2/2002	4/1/2004
Cooling Tower Electrical Redundancy	1/2/2002	4/1/2004
Unit 1 Projects	1/2/2001	4/2/2003
HP Turbine Retrofit	1/15/2001	4/1/2003
Cooling Tower Performance Upgrade	2/1/2001	4/1/2003
Boiler Safety Valve Addition	3/1/2001	4/1/2003
Generator Cooling Enhancements	1/2/2002	4/2/2003
Isophase Cooling Enhancements	1/2/2002	4/2/2003
Large Motor Bus Loading Equalization	1/2/2002	4/1/2003
Boiler Feed Pump Performance Upgrade	1/2/2001	4/1/2003
Main Step-up Transformer Cooling	1/2/2002	4/1/2003
NOx Reduction Project	3/1/2001	4/1/2003
Scrubber Wall Ring	5/1/2001	4/1/2003
Generator SCW O2 Monitoring	1/2/2002	4/1/2003
HP Heater Drain Line Mods	4/2/2001	3/1/2002
Boiler Modifications	4/2/2001	4/1/2003
Cooling Tower Electrical Redundancy	1/2/2002	3/31/2003

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